

# Performance Evaluation in Conventional and Rectenna Solar Cells

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2015-present



2013-2014



2011-2013



2006-2011



# First Solar 10GW INSTALLED WORLDWIDE



Enough panels to circle *THE EARTH*  
**3.5 TIMES**

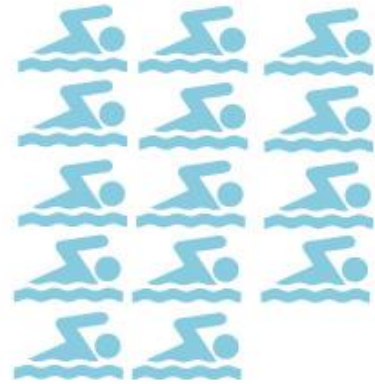


Enough to power  
**WASHINGTON D.C.**  
for *A YEAR*

Equivalent to **7,000**  
*OLYMPIC* swimming pools



*POWER* for **5,000,000**  
average homes



**= 500 SWIMMING  
POOLS**



**18,000,000,000**  
liters of water  
*SAVED*



**= 100,000 HOMES**



San Luis Obispo County,  
California

Customer: MidAmerican

Size: 550MW (AC)

Construction Time: 2011—2015

Acres: ~7,800 site

Modules: ~9 million



**Cars Removed:**

73,000



**Tons CO<sub>2</sub> Displaced  
Annually:**

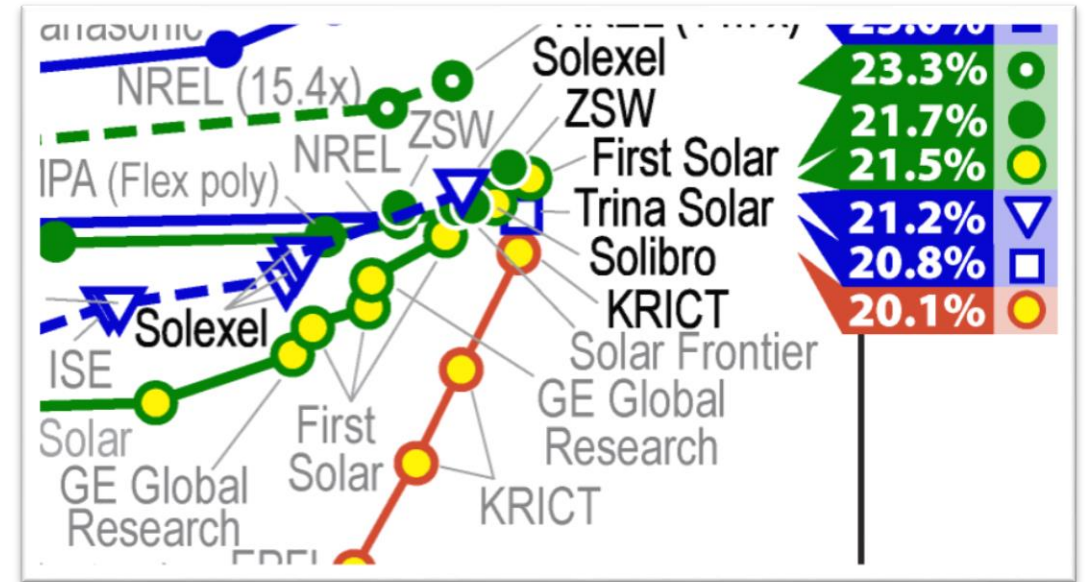
377,000

**TOPAZ SOLAR FARM**

# Record efficiency: 18.6% aperture area efficiency (18.2% full area)

"At one time, we might have been characterized as a low cost, low efficiency technology, but consistent with our technology projections we are now proving that CdTe thin film delivers both industry-leading performance AND sustainable thin-film cost structures."

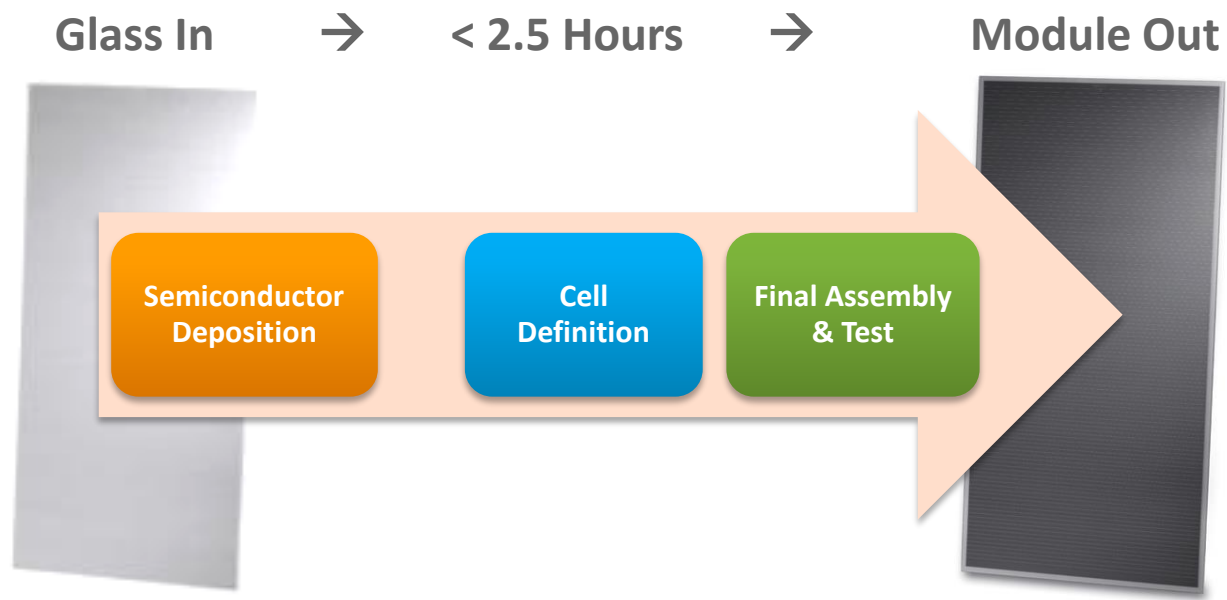
-Raffi Garabedian, First Solar CTO



<http://investor.firstsolar.com/releasedetail.cfm?ReleaseID=917926>  
[http://www.nrel.gov/ncpv/images/efficiency\\_chart.jpg](http://www.nrel.gov/ncpv/images/efficiency_chart.jpg)

# PV Module technology & manufacturing

## First Solar Fully Integrated, Automated and Continuous Thin Film (CdTe) Process



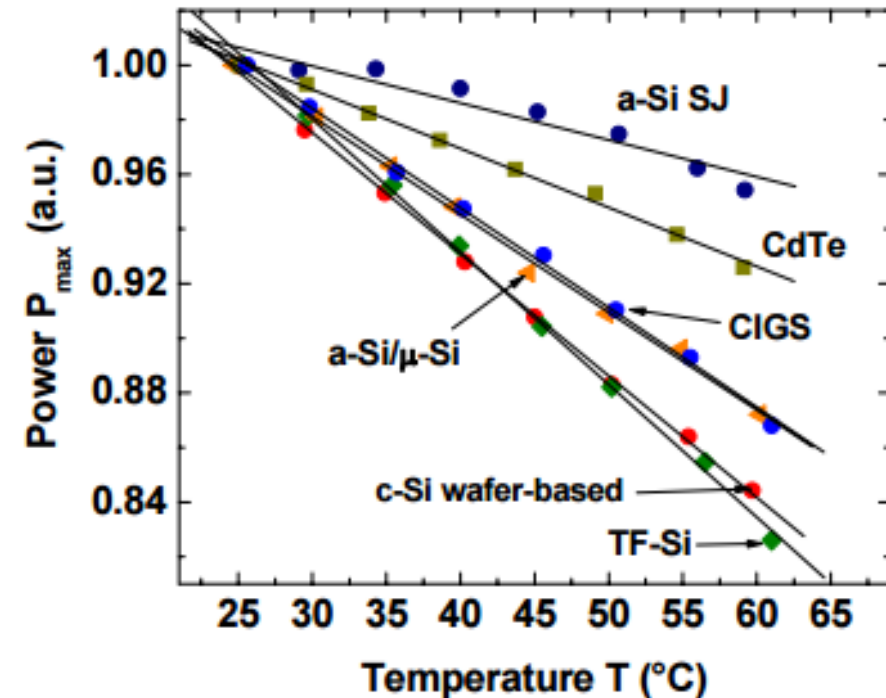
- 98-99% reduction in semiconductor material
  - Direct bandgap material
- Fully integrated, continuous process vs. batch processing
- Large 60 x 120cm (2' x 4') superstrate vs. 6" wafers

## Conventional Crystalline Silicon Batch Technology



# Superior Temperature Coefficient of CdTe yields more energy

- Temperate Climate Example:
  - Module Temps often reach 65° C; 40° C above the STC rating
  - The silicon module power output will be reduced by up to 20% at this temperature
  - FSLR output will be reduced by only 10%
- Hot Climate:
  - More hours at higher temps (Module temps can reach 85° C)
  - FS Advantage grows more pronounced

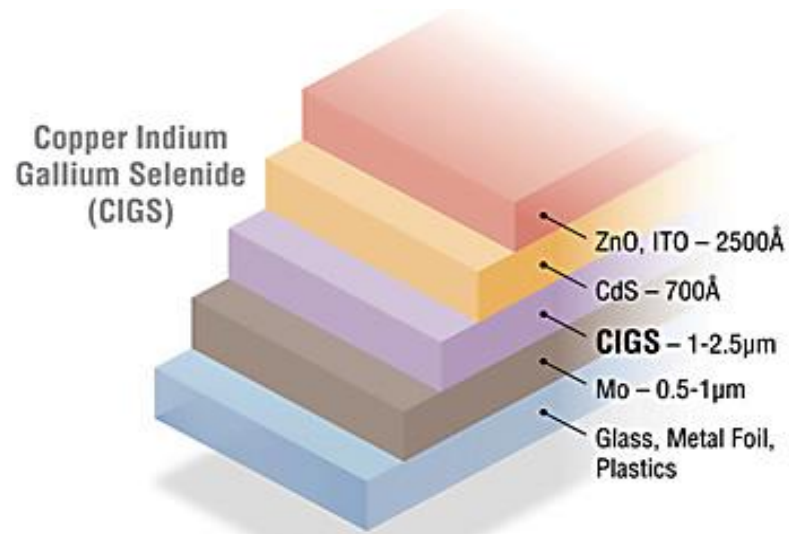


Virtuani, 25<sup>th</sup> EUPVSEC, 2010

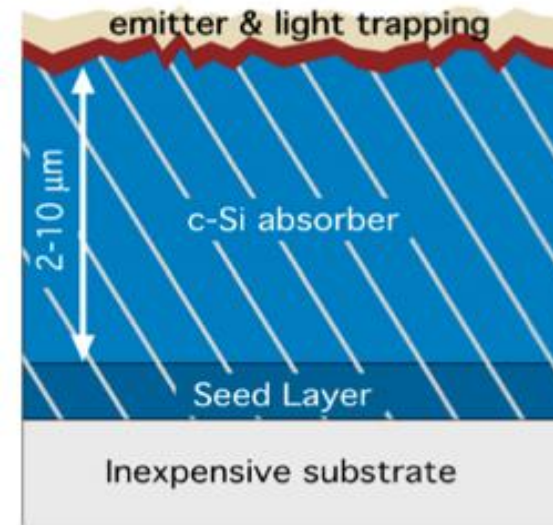
## Outline

- Derive theoretical dependence of  $V_{OC}$  on
  - Light intensity
  - Temperature
  - Strength of recombination channels
- Apply formulation to
  - Quantify recombination in different regions of the cell
  - Extract material and interface quality

# Express $V_{OC}$ in terms of SRH recombination in different regions



CIGS solar cell  
Rau, *Appl. Phys. A* 69, 1999

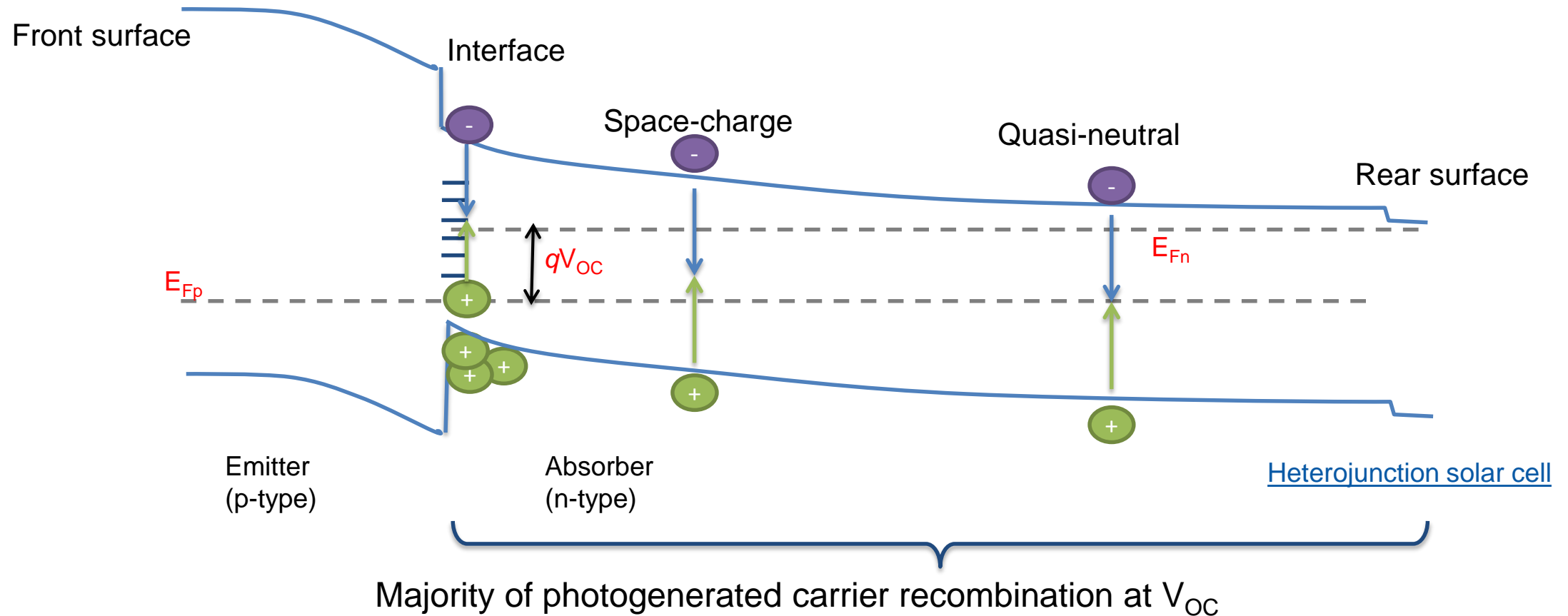


Epitaxial silicon heterojunction  
Branz, *Thin Solid Films*, 519, 2011

Quantitative estimate of (microscopic) recombination from conventional (macroscopic) measurements



# Recombination → Quasi-Fermi separation → $V_{OC}$



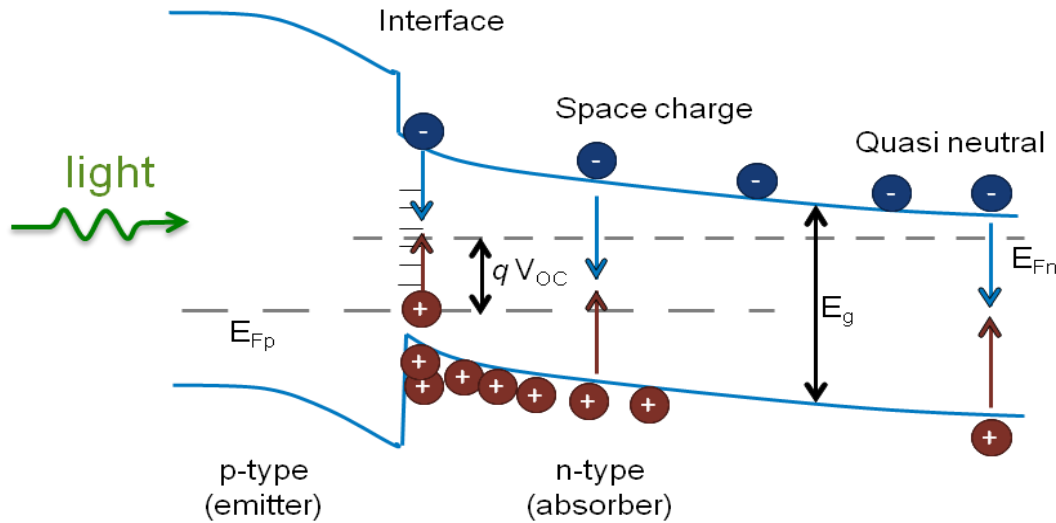
$$V_{oc} = \frac{kT}{q} \ln \left( \frac{J_{sc}}{J_{o,total}} + 1 \right)$$

Not precise but workable!

Loss of exact dependences on recombination mechanisms

$$J_{o,total} = J_{o,Radiation} + J_{o,Auger} + J_{o,SRH} + J_{o,emitter} + J_{o,rear}$$

# Relating $V_{OC}$ to carrier concentrations via $\beta$



How to think of  $V_{OC}$  in this analysis:

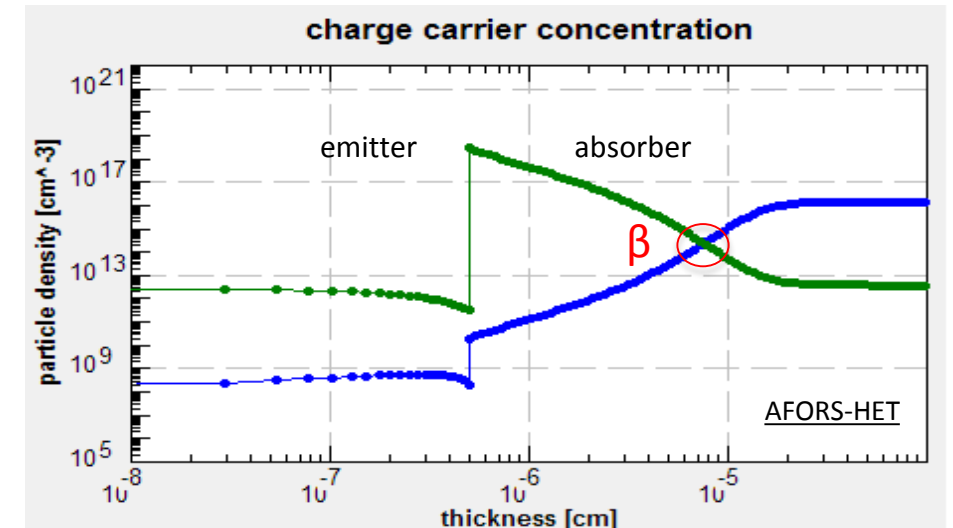
- Not a performance metric but a variable
- Depends on light intensity, temperature, and recombination
- Constant or near constant throughout the cell
  - Breaks down for very strong recombination

$$V_{OC} = E_{Fn} - E_{Fp} = \frac{kT}{q} \ln\left(\frac{n_e p_h}{n_i^2}\right) = \frac{kT}{q} \ln(\beta^2)$$

For constant QFL separation,  $\beta$  is constant across cell

$$\beta^2 = N_D \Delta p / n_i^2 \quad \text{in quasi-neutral region}$$

$\beta$  can similarly be used to relate  $n_e$  and  $p_h$  at interface



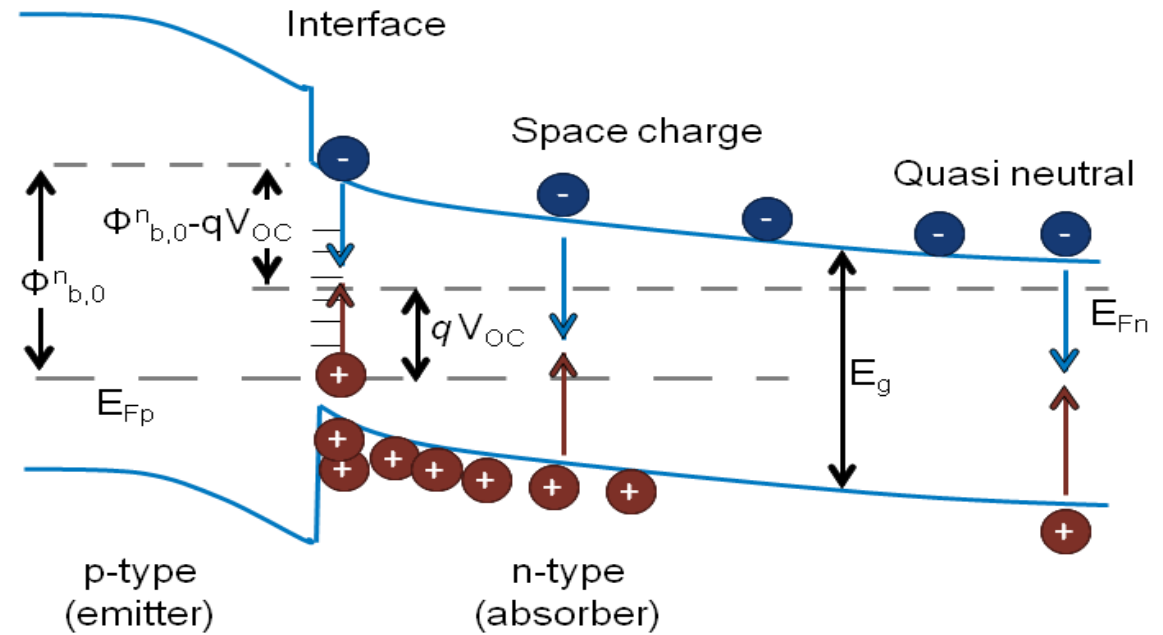
# Recombination rate depends on limited availability of carriers

## Rate limiting carrier type:

*Interface:* electrons

*Quasi-neutral:* holes

*Space-charge:* both



- Express recombination in terms of  $\beta$
- Recombination
  - Rate per unit volume:  $U_{SRH}$
  - Rate integrated over thickness:  $R_{SRH} = U_{SRH} \cdot \text{thickness}$
- Equate generation and recombination  $G^*W = \sum R_{SRH}$ 
  - $G^*W = J_{ph}$

# Defining all recombination with common $\beta$

- Simplified SRH equation: 
$$U_{SRH} = \frac{np}{\tau_p n + \tau_n p}$$

- Quasi-neutral/Bulk (n=1)

- $N_D \gg \Delta p$
- Activation:  $E_g$

$$R^b = W_b U_{SRH}^b = W_b \frac{\Delta p}{\tau_p} = \left( \frac{W_b n_i^2}{N_D \tau_p} \right) \beta^2 = R_0^b \beta^2$$

- Interface (n=1)

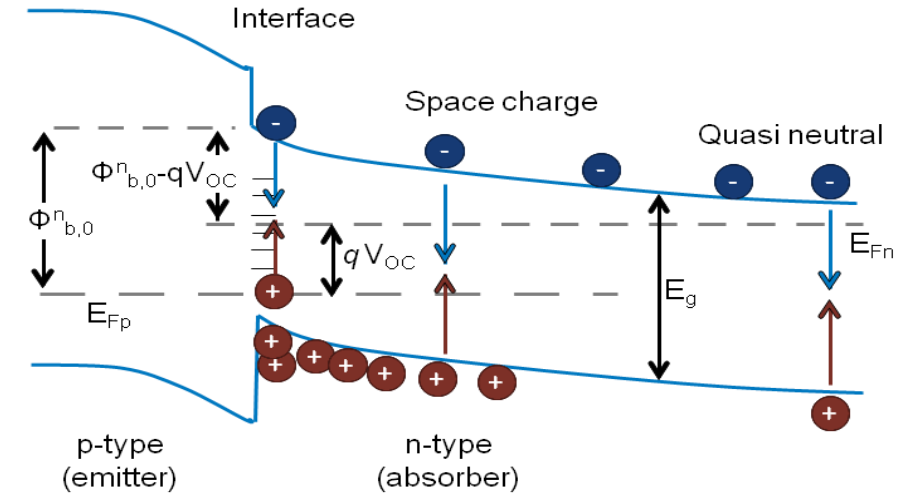
- $p \gg n$
- Activation:  $\Phi_{b,0}^n$

$$R^I = S_n n_e = S_n N_C \exp \left\{ - \frac{\Phi_{b,0}^n}{kT} \right\} \beta^2 = R_0^I \beta^2$$

- Space charge (n=2)

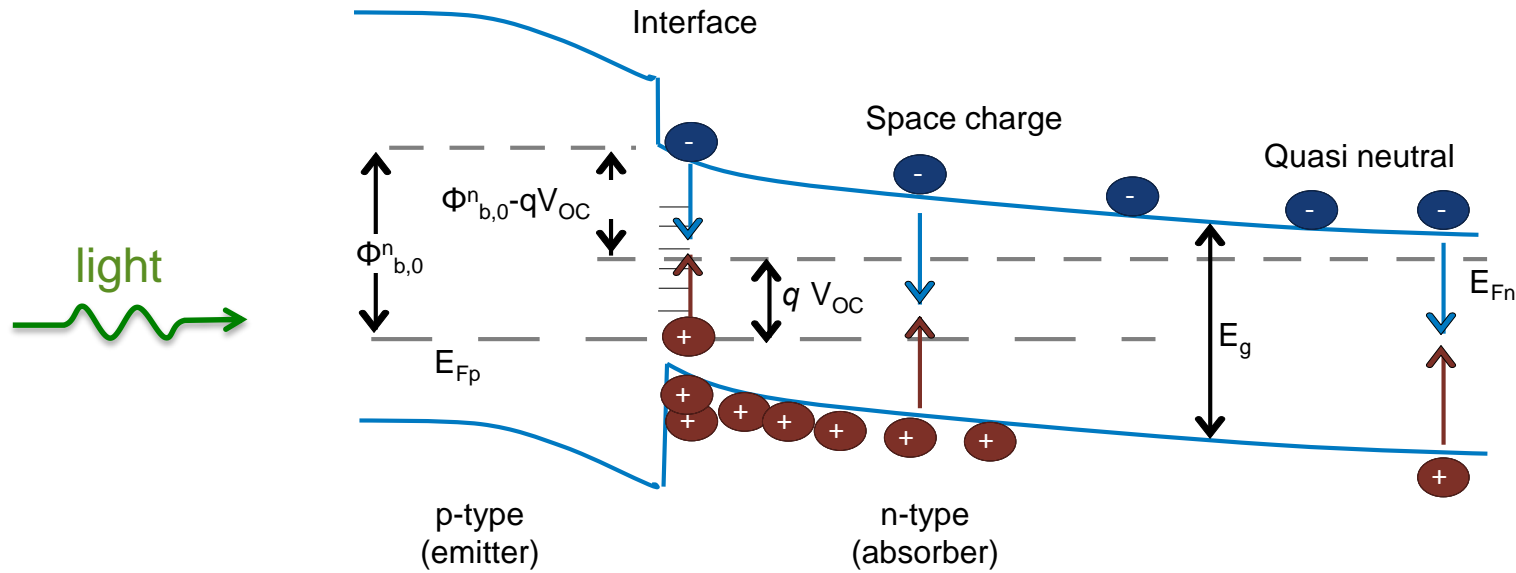
- $p \approx n$
- Activation:  $E_g$

$$R^d = W_d U_{SRH}^d = \left( \frac{W_d n_i}{\tau_p + \tau_n} \right) \beta = R_0^d \beta$$



Scheer, JAP, 105, 104505, 2009

# Recombination = Generation



$$R^b + R^I + R^d = \int_W G_x dx = G_{avg} W$$

$$R_0^b b^2 + R_0^I b^2 + R_0^d b = \int_W G_x dx = G_{avg} W$$

Solve quadratic to obtain  $\beta$  &  $V_{OC}$

$$V_{OC} = 2 \frac{kT}{q} \ln \left[ \frac{k_1 \left[ \sqrt{1 + k_2 G_{avg}} - 1 \right]}{n_i} \right]$$

$V_{OC}$  dependence on:

- Operating conditions: light intensity, temperature
- Strength of SRH recombination in bulk, interface, and depletion

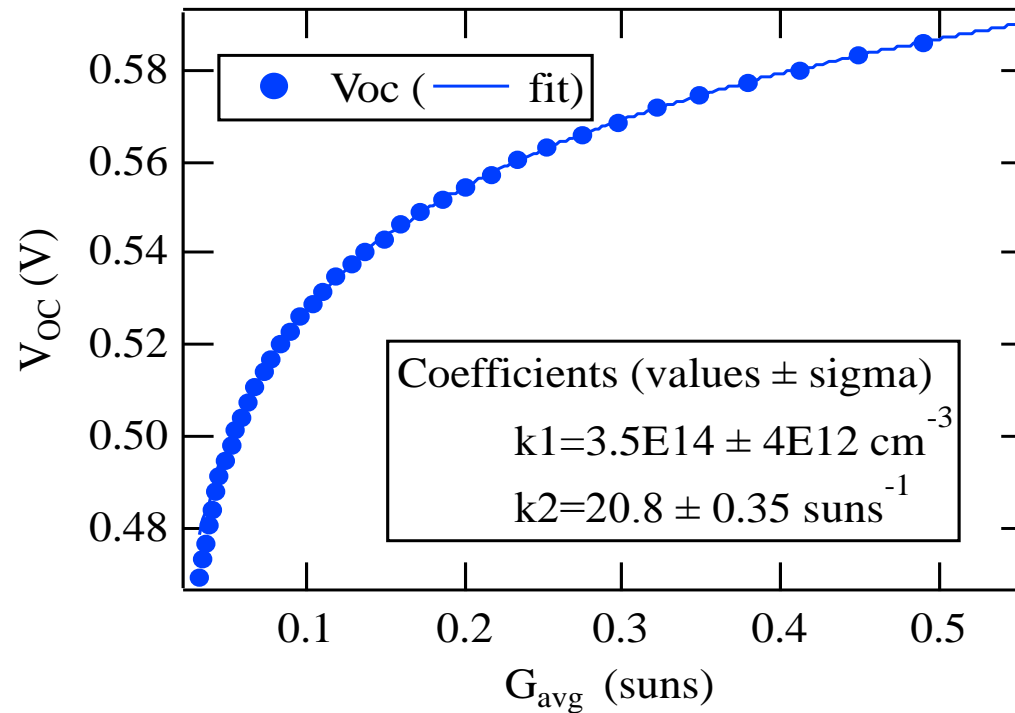
$$k_1 = \frac{R_0^d}{2(R_0^I + R_0^b)}; \quad k_2 = 4W \frac{(R_0^I + R_0^b)}{(R_0^d)^2}.$$

$$= W_b \frac{\Delta p}{\tau_p} = \left( \frac{W_b n_i^2}{N_D \tau_p} \right) \beta^2 = R_0^b \beta^2$$

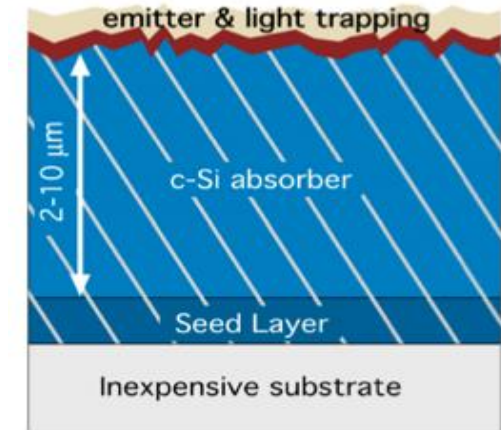
$$: S_n N_C \exp \left\{ -\frac{\phi_{b,0}^n}{kT} \right\} \beta^2 = R_0^I \beta^2$$

$$W_d U_{SRH}^d = \left( \frac{W_d n_i}{\tau_p + \tau_n} \right) \beta = R_0^d \beta$$

# Fitting the light intensity dependence of $V_{OC}$



Measured light-intensity dependence of  $V_{OC}$



a-Si/c-Si heterojunction solar cell using heteroepitaxial silicon film

Convert light intensity  $\rightarrow$  generation rate

$$V_{OC} = 2 \frac{kT}{q} \ln \left[ \frac{k_1 \left[ \sqrt{1 + k_2 G_{avg}} - 1 \right]}{n_i} \right]$$

$$k_1 = \frac{R_0^d}{2(R_0^l + R_0^b)}; \quad k_2 = 4W \frac{(R_0^l + R_0^b)}{(R_0^d)^2}$$

# Define and fit ideality factor ( $n$ )

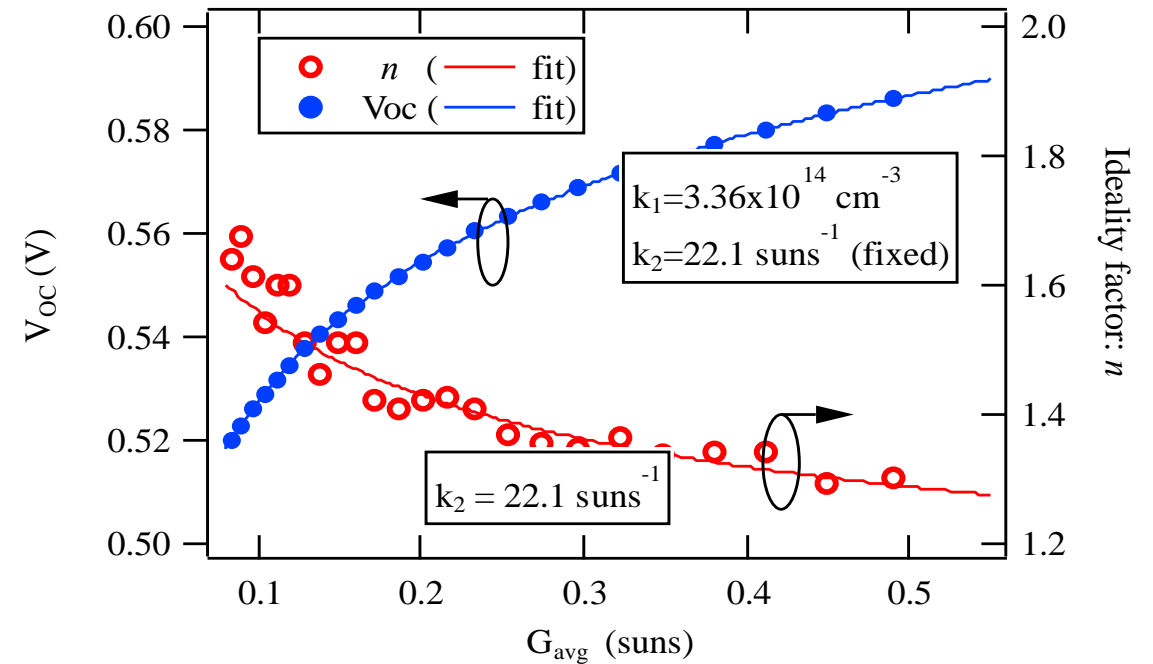
$$n = \left[ \frac{kT}{q} \frac{d \ln G_{avg}}{dV_{OC}} \right]^{-1}$$

$$n(G_{avg}) = \frac{k_2 G_{avg}}{\sqrt{1 + k_2 G_{avg}} \left[ \sqrt{1 + k_2 G_{avg}} - 1 \right]}$$

$$n \{ k_2 G_{avg} \rightarrow 0 \} = 2$$

$$n \{ k_2 G_{avg} \rightarrow \infty \} = 1$$

$k_1$  &  $k_2$  are sufficient for quantifying recombination in absence of interface





# Defining activation energy from $V_{OC}(T)$ extrapolation

## Linear extrapolation of $V_{OC}(T)$

$$V_{OC}(T_R) = \frac{E_a}{q} + T_R \left. \frac{dV_{OC}}{dT} \right|_{T_R}$$

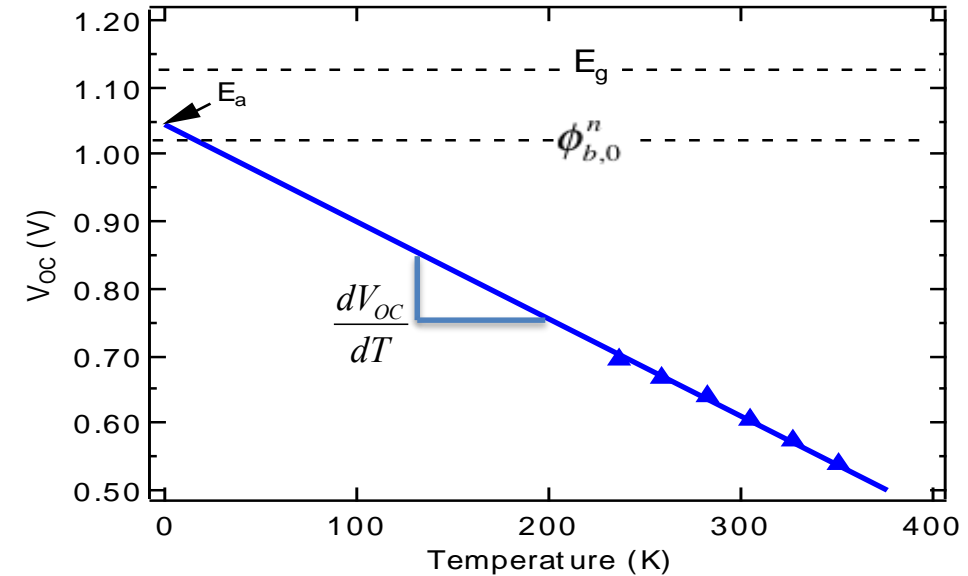
## Substitute explicit dependence of $V_{OC}$ on T

$$V_{OC} = 2 \frac{kT}{q} \ln \left[ \frac{k_1 \left[ \sqrt{1 + k_2 G_{avg}} - 1 \right]}{n_i} \right]$$

Assuming  $k_2 G_{avg} \gg 1$  (negligible SCR, large fwd. bias):

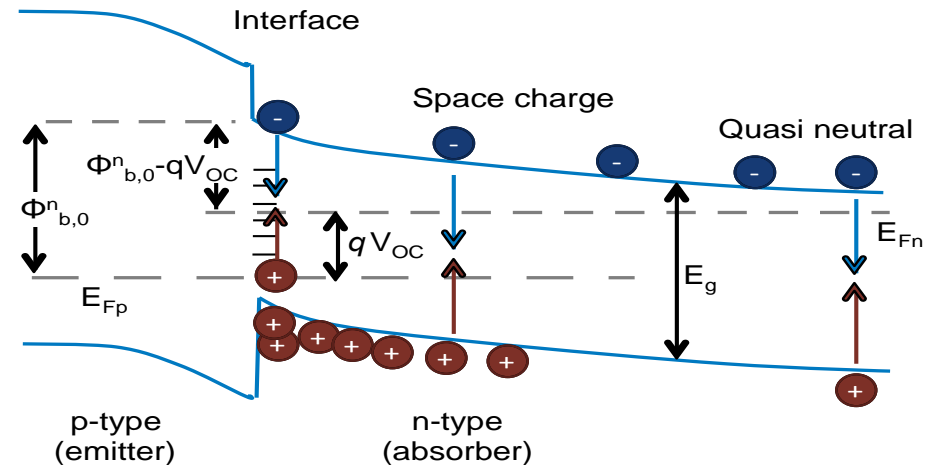
$$E_a = \frac{R_0^b E_g(T_R) + R_0^I \phi_{b,0}^n(T_R)}{R_0^b + R_0^I}$$

Weighted mean of activation energies  
Weights = strength of recombination

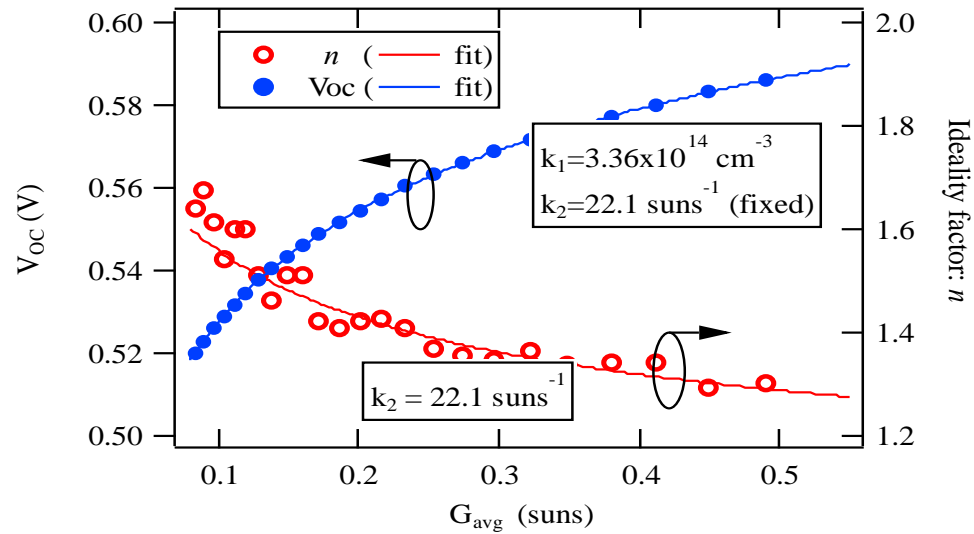


## Extrapolated temperature dependence

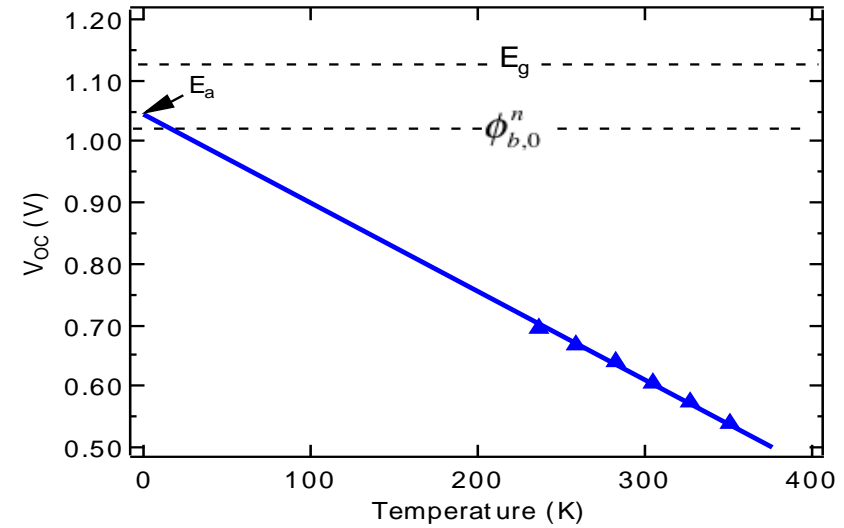
$E_a \neq E_g$  linked to interface recombination



# Quantifying recombination in different regions

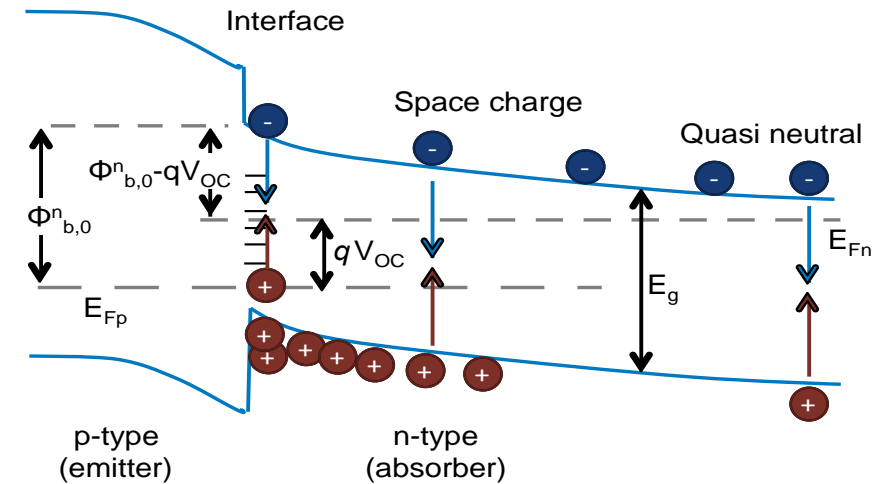


Light-intensity variation

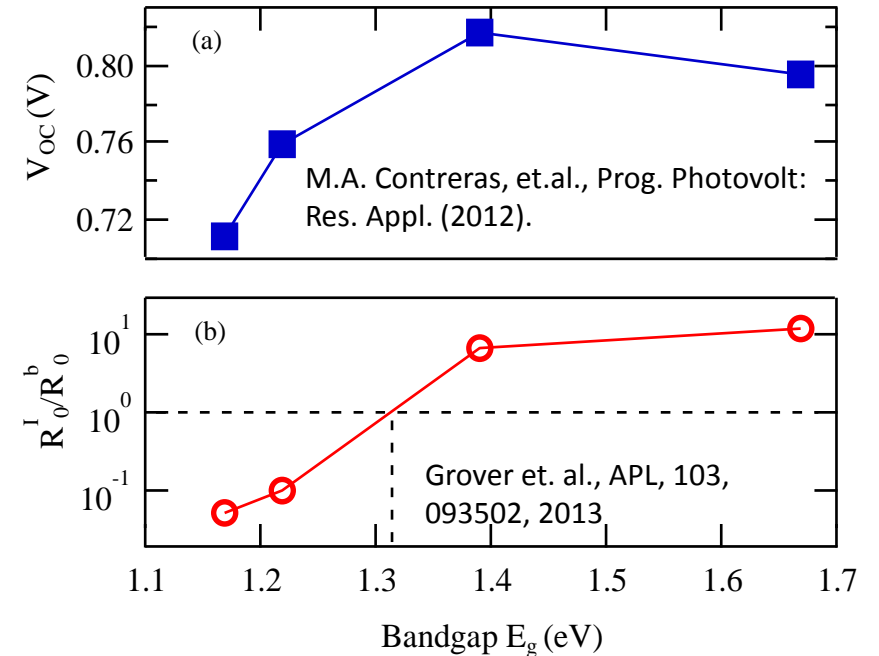
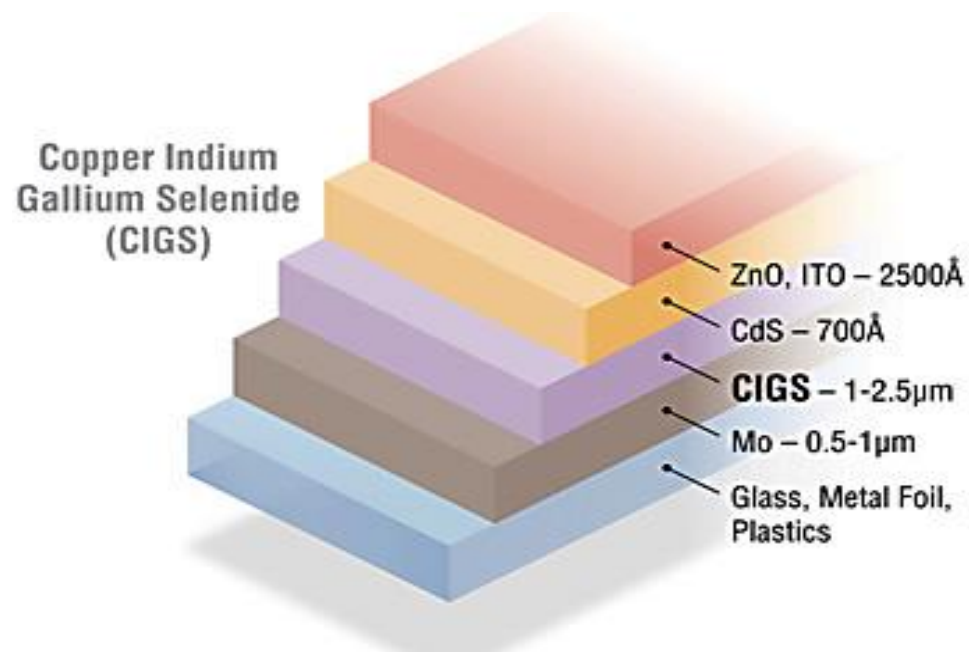


Extrapolated temperature dependence

$$\left\{ \begin{array}{l} k_1 \\ k_2 \\ E_a \end{array} \right\} \xrightarrow{\frac{V_{OC}(T,G)}{C(V)}} \left\{ \begin{array}{l} R^b = 16\% \\ R^d = 46\% \\ R^I = 38\% \end{array} \right\} \text{ at 1 sun}$$



# Recombination analysis in CIGS cells with varying [Ga]

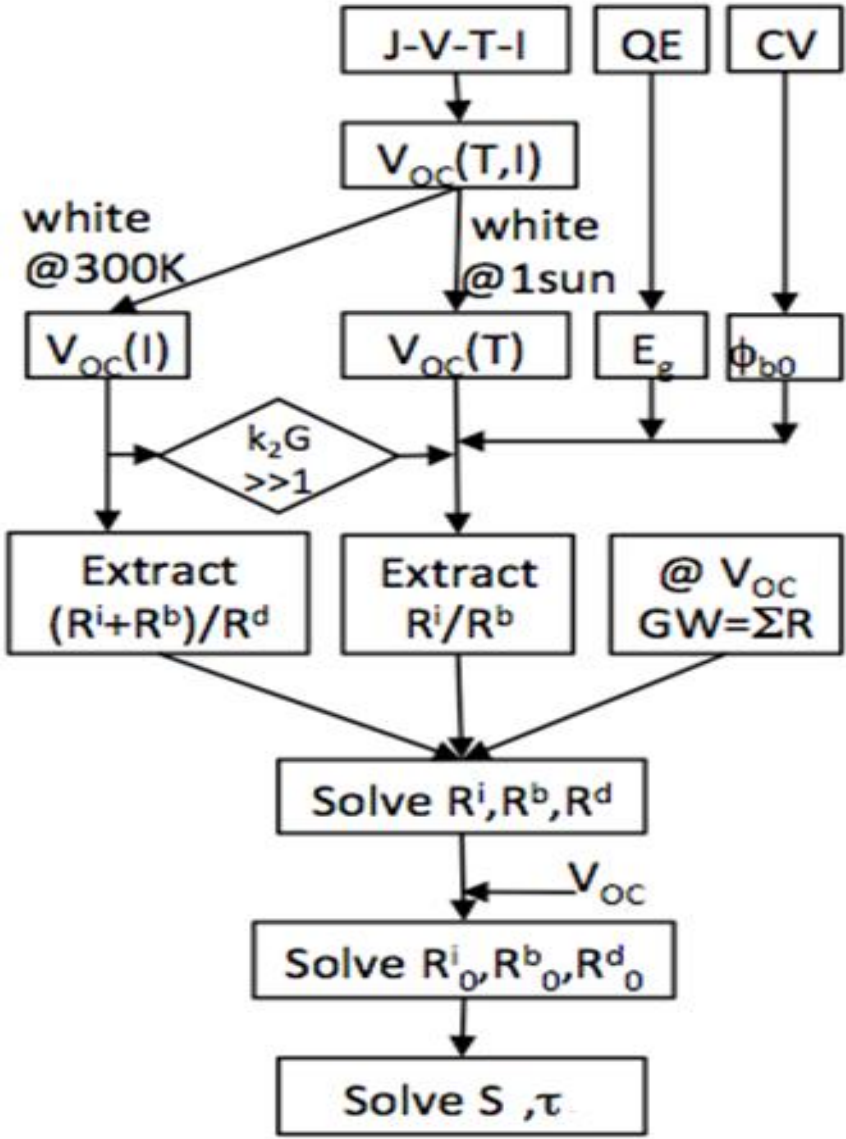


(a):  $V_{oc}$  vs. bandgap ( $E_g$ ) for CIGS solar cells.  $V_{oc}$  saturates as  $E_g$  increases with increasing Ga content. (b): Ratio of interface ( $R'_o$ ) and bulk ( $R^b_o$ ) recombination strengths increases dramatically for the higher bandgap samples.

- Agreement of lifetime obtained from  $V_{oc}(T,I)$  and TRPL
- Successfully tracks nuances of recombination variations based on material properties

Li et al., A recombination analysis of CIGS solar cells with low and high Ga compositions, *Sol. Energy Mat. and Sol. Cells*, 124 (2014) 143-149

# Procedure for calculation of recombination rates



# New equation for temperature coefficient of $V_{OC}$

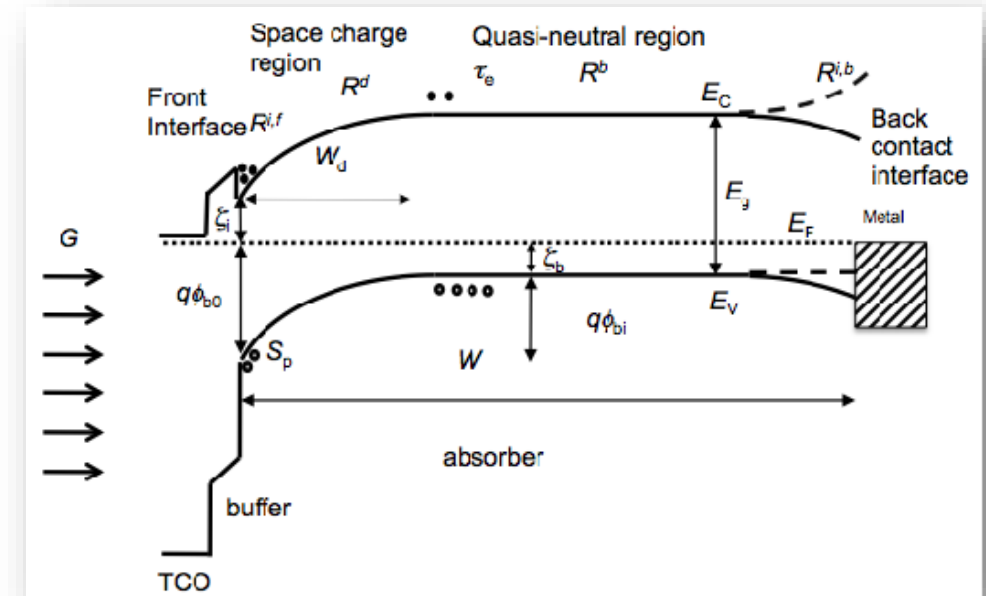
$$\frac{dV_{OC}}{dT} = -\frac{1}{T} \left[ \frac{nE_g}{mq} - V_{OC} + \frac{\gamma nkT}{q} \right]$$

Green, PIP, 11(5),  
333–340, 2003

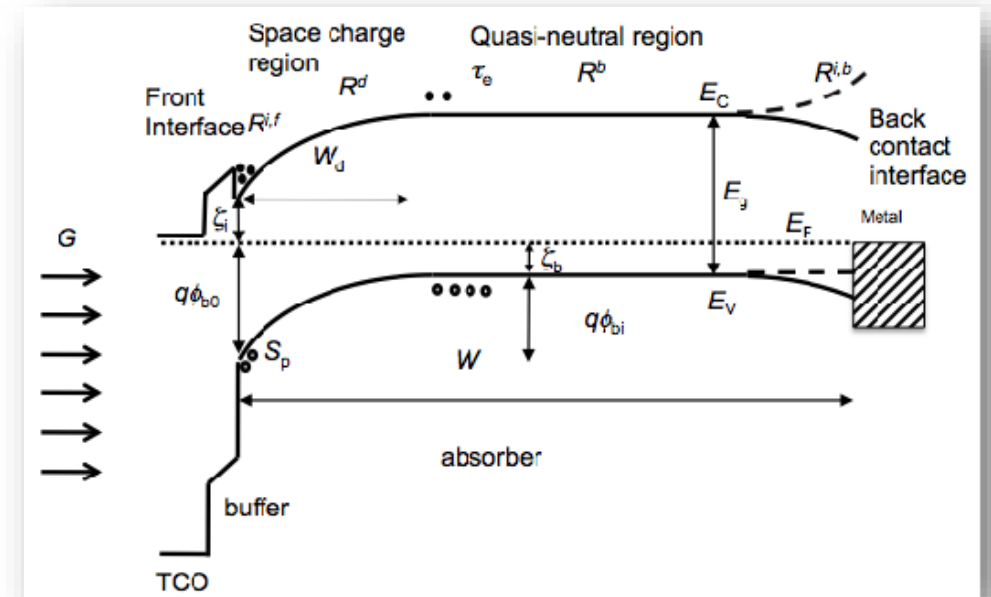
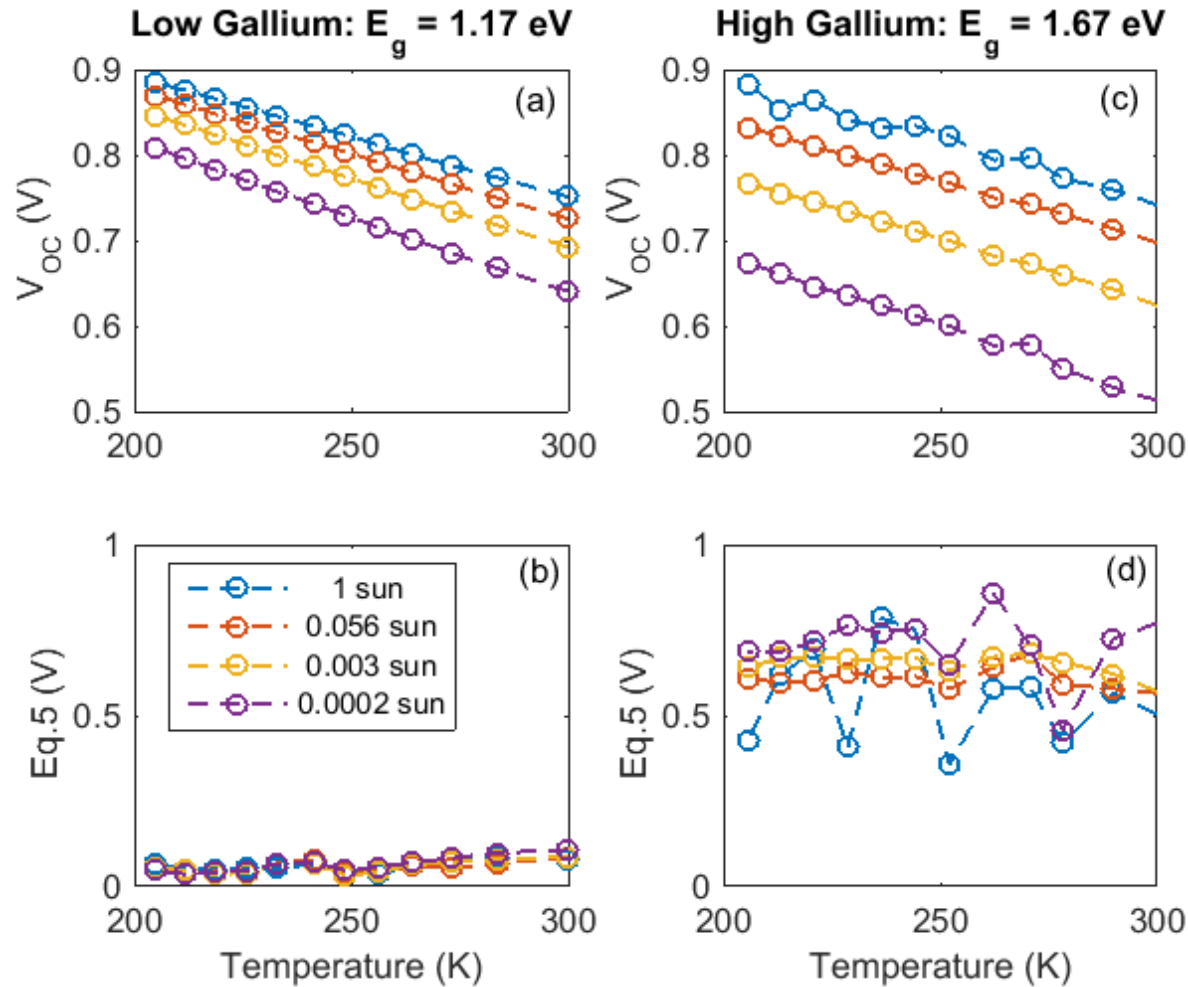
- $n$  – ideality factor; combines all recombination channels
- $n/m$  – experimental fitting parameter

$$\frac{dV_{OC}}{dT} = -\frac{1}{T} \left[ \frac{E_g}{q} \left\{ 1 + \frac{\alpha T (T + 2\beta)}{(T + \beta)^2} \right\} - V_{OC} + \frac{\gamma kT}{q} - \frac{(2-n)R_0^i}{(R_0^i + R_0^b)} \frac{\zeta_i}{q} \right]$$

- $V_{OC}$  depends on interface recombination and Fermi-pinning
- Smaller  $V_{OC}$  for larger interface recombination → not necessarily good



# High [Ga] CIGS cells are interface limited

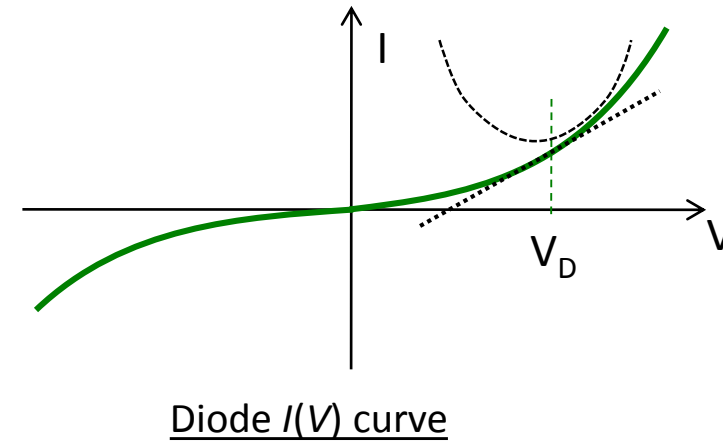
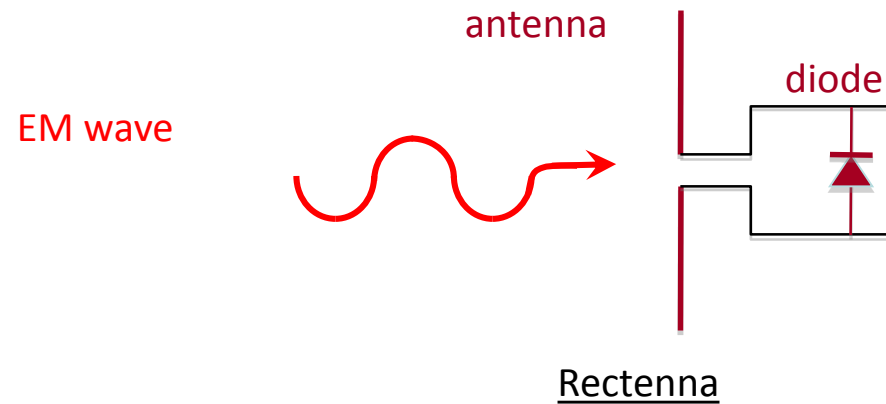


Rearrange terms to calculate interface contribution:

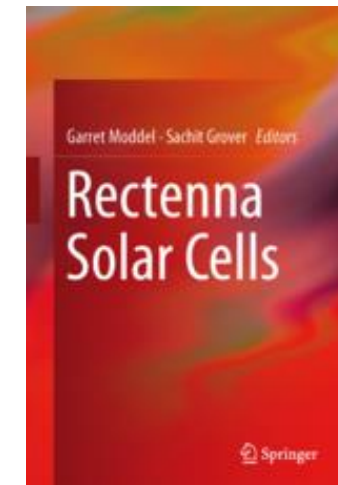
$$\frac{(2-n)R_0^i}{(R_0^i + R_0^b)} \frac{\zeta_i}{q} = T \frac{dV_{OC}}{dT} + \left[ \frac{E_g}{q} - V_{OC} + \frac{\gamma kT}{q} \right]$$

# Questions so far?

# Operating Principle of Rectennas

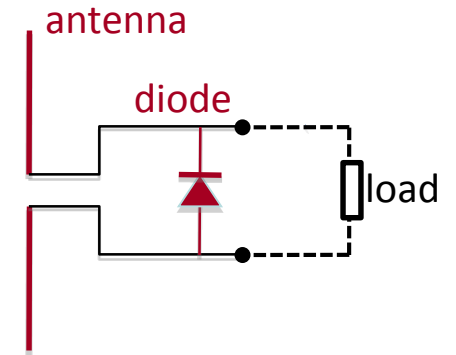
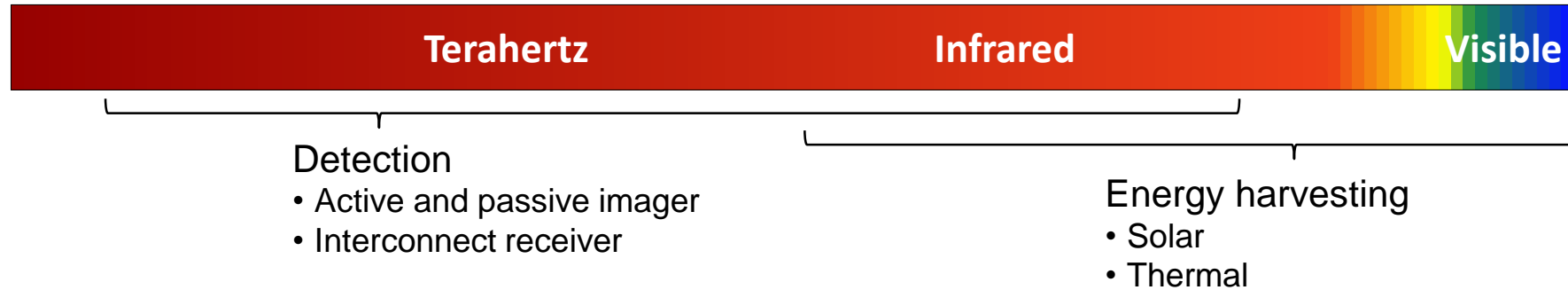


- Square-law rectification
  - Signal strength smaller than diode switching voltage
    - 1 mV for 1 sun incident over  $1 \mu\text{m}^2$  and  $100 \Omega$  antenna
- Key diode parameters
  - Resistance ( $R_D$ ), responsivity ( $\beta_i$ )



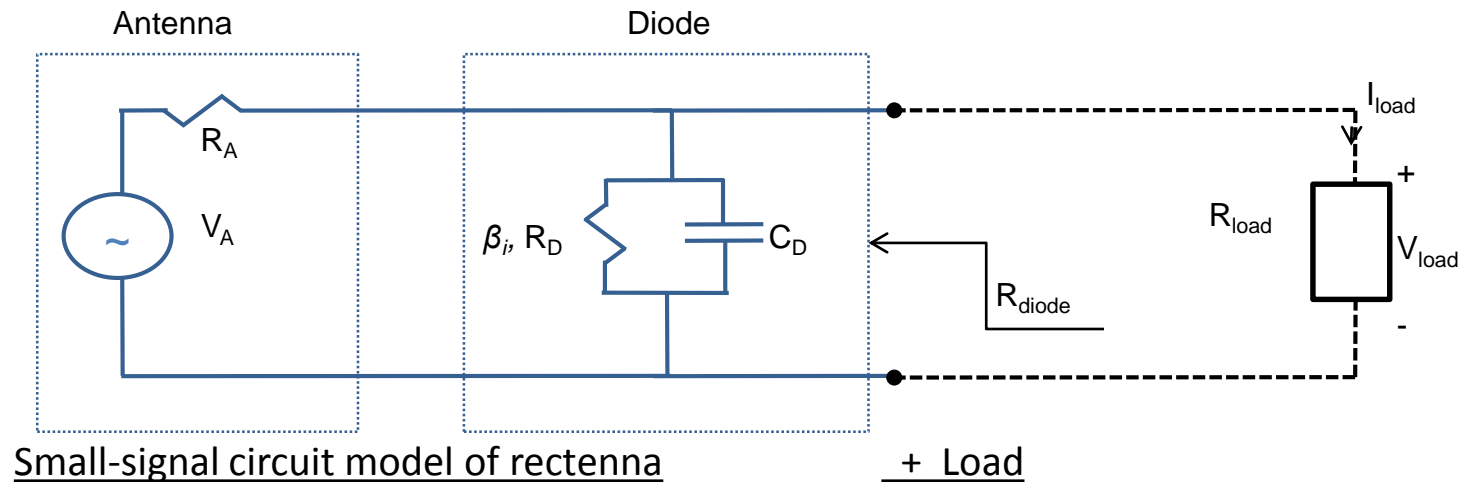


- Spectral range and applications



- Potential for high-efficiency low-cost
  - 90% efficient microwave rectennas exist
    - Large-signal: diode operates as switch
- Current state
  - IR detectors demonstrated (Q.E.  $\sim 0.01\%$  @  $10.6 \mu\text{m}$ )\*
  - Solar cells proposed in 1972, no practical demonstration as yet

# Requirements for Efficient Rectennas



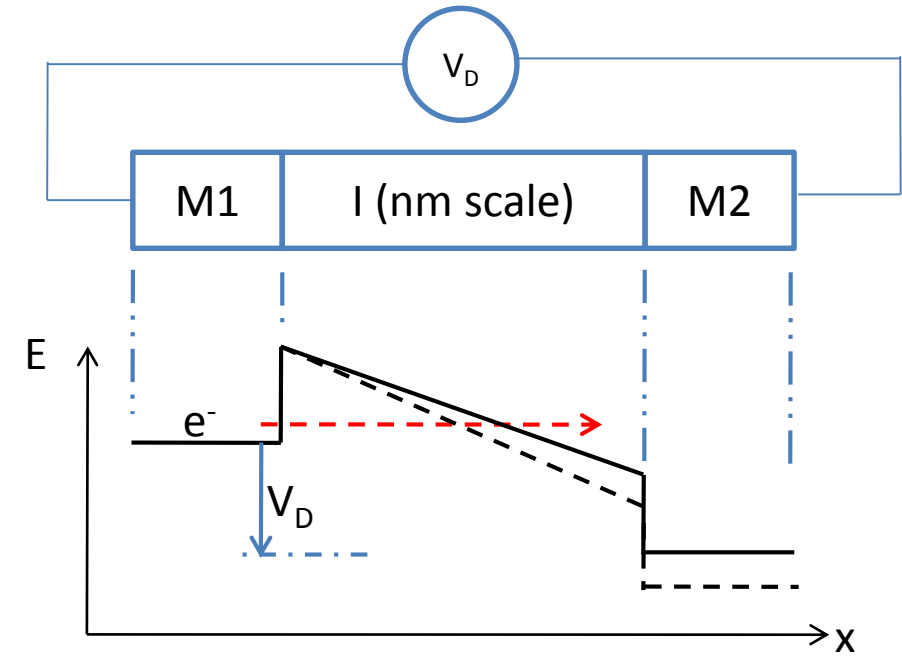
- Intrinsically fast diode
- Low  $R_D$  to match to  $R_A$
- Low  $C_D$  to prevent shunting  $R_D$
- High  $\beta_i$  for rectification
- Large  $V_A$  for high power-conversion efficiency
- Efficient antennas

Antenna to diode coupling

Field enhancement

Diode design

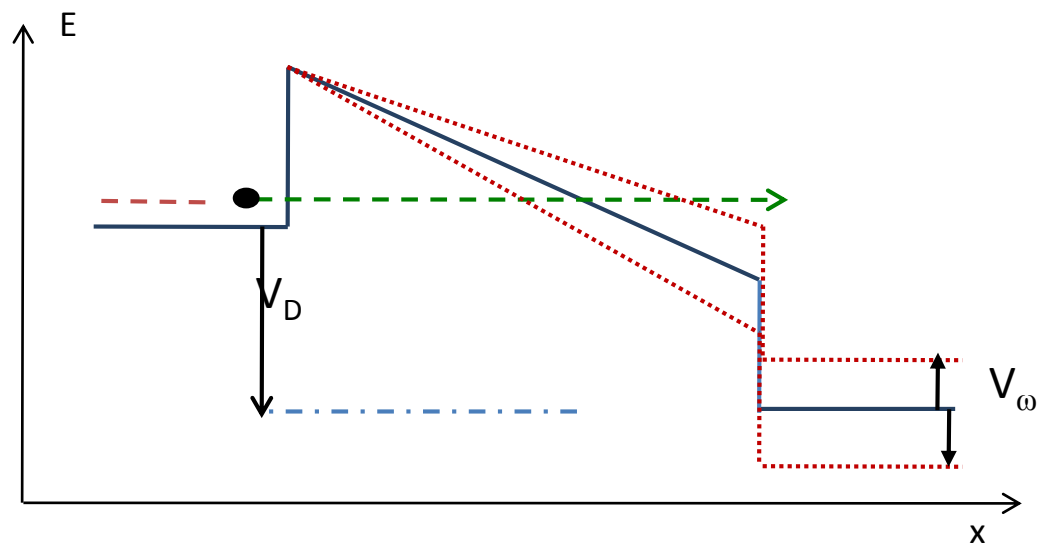
- Mechanism
  - Tunneling across thin insulator
    - Nonlinear  $I(V)$
    - Femtosecond fast
- Summary of work done
  - Fabrication
    - Sputtered metals and insulators
  - Simulation
    - Transfer matrix method
  - Modification
    - Field effect transistor
    - Double-insulator (MIIM) barrier design



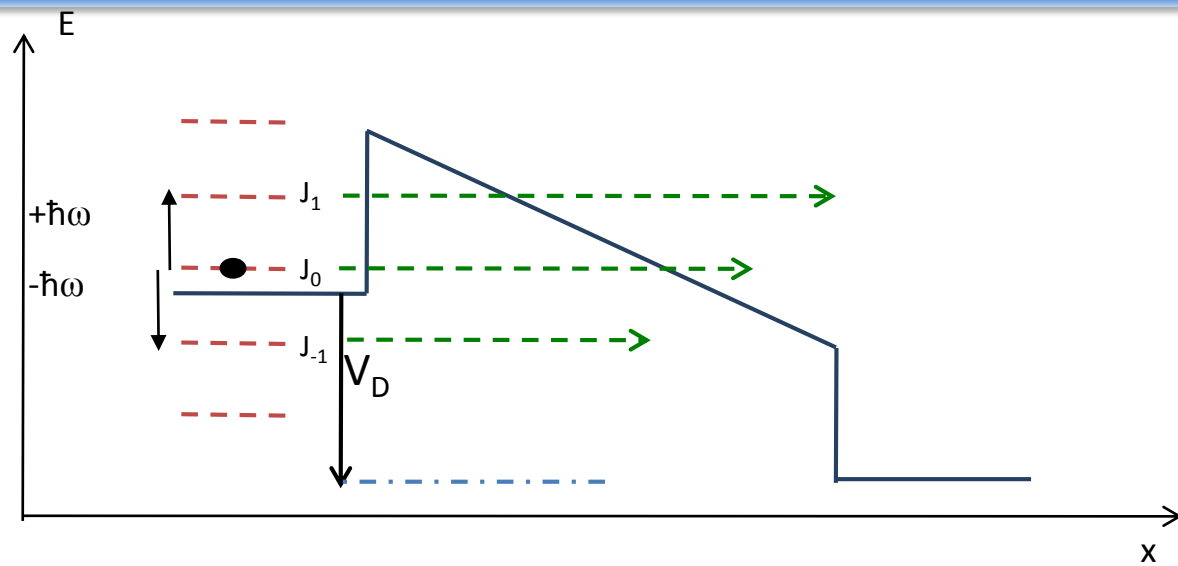
MIM diode energy-band profile

Grover, Ph.D. Thesis, CU Boulder, 2011

# Semiclassical Theory of Rectification in MIM



Classical: low frequency

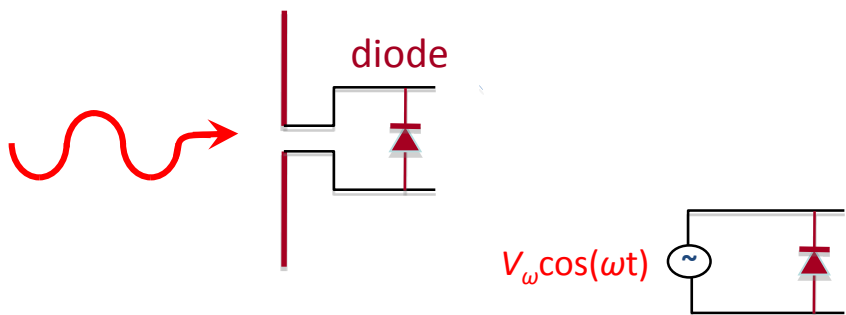


Semiclassical: high frequency

Photon-assisted transport applies when  $\hbar\omega/e$   
 $\sim$  voltage-scale of diode nonlinearity

DC  $I(V)$  under illumination:

$$I_{illum}(V_D, V_\omega) = \sum_{n=-\infty}^{\infty} J_n^2(\alpha) I_{dark}\left(V_D + n \frac{\hbar\omega}{e}\right); \quad \alpha = \frac{eV_\omega}{\hbar\omega}$$



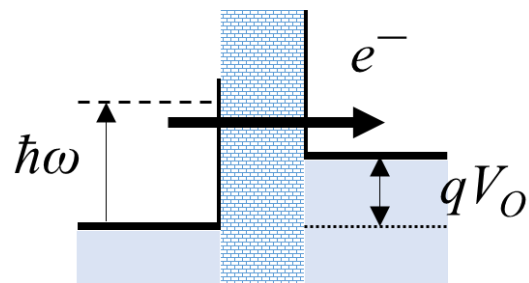
Grover, et.al, J. Phys D., 46 (13), 135106, 2013;  
 Tien, Gordon, Phys. Rev., 129(2), 1963

# Efficiency limit for monochromatic response of rectenna

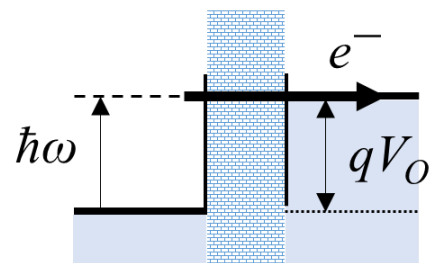
Slide courtesy: Saumil Joshi, UC Boulder

- Assume ideal diode – high fwd/rev asymmetry
- 1  $\mu\text{W}$  input (low intensity regime) – 1 photon process
- $|V_O| < \hbar\omega/q$ , 1photon/1electron

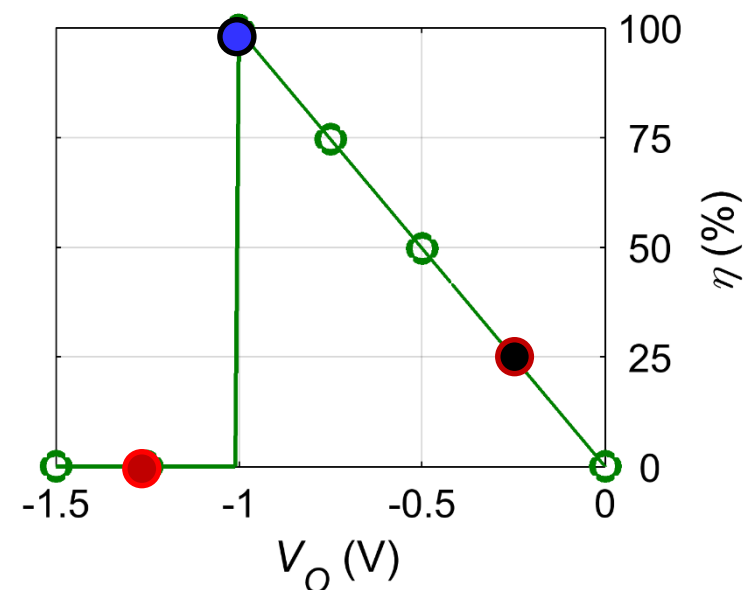
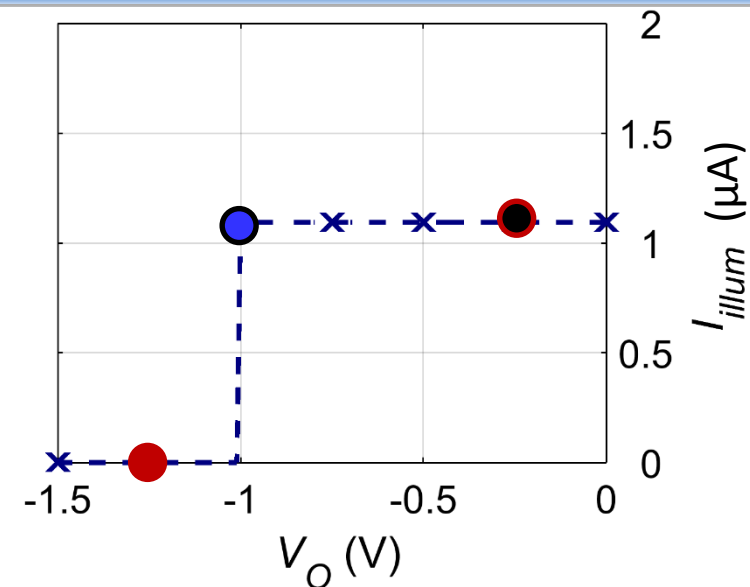
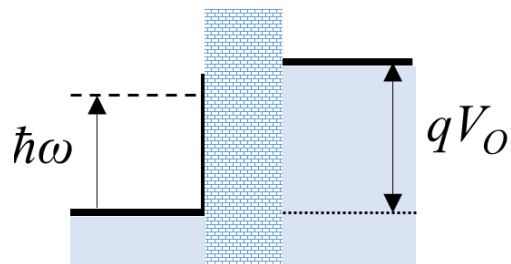
$|V_O| < \hbar\omega/q$



$|V_O| = \hbar\omega/q$



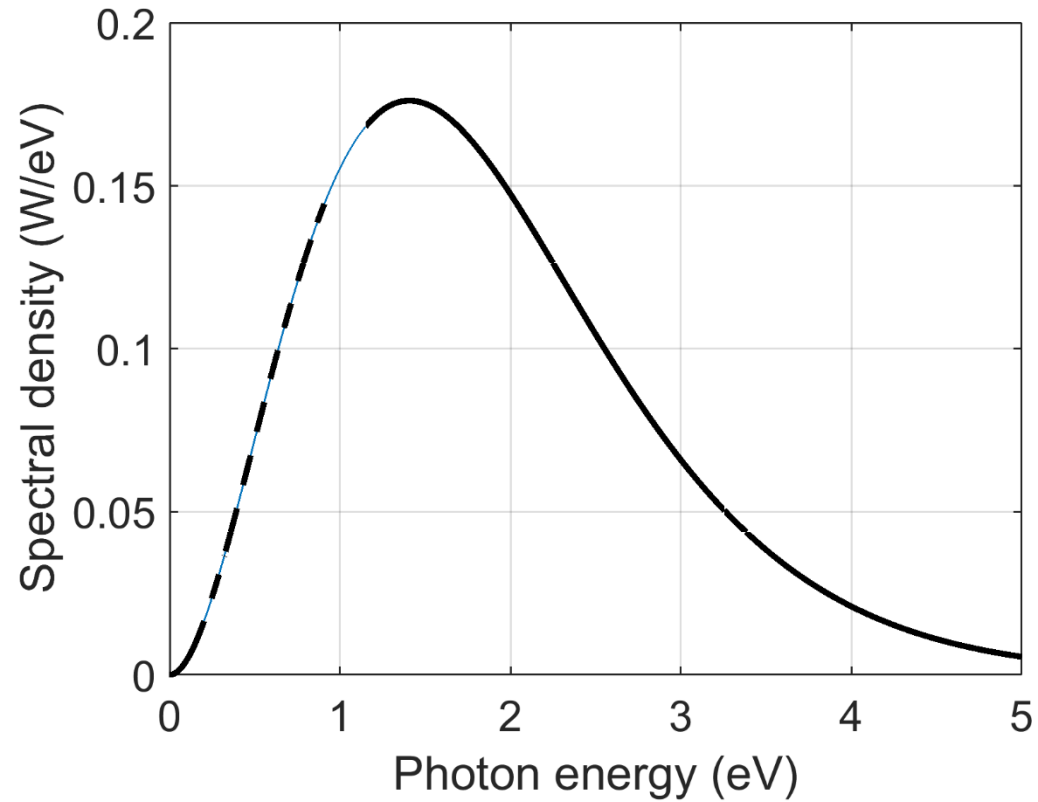
$|V_O| > \hbar\omega/q$



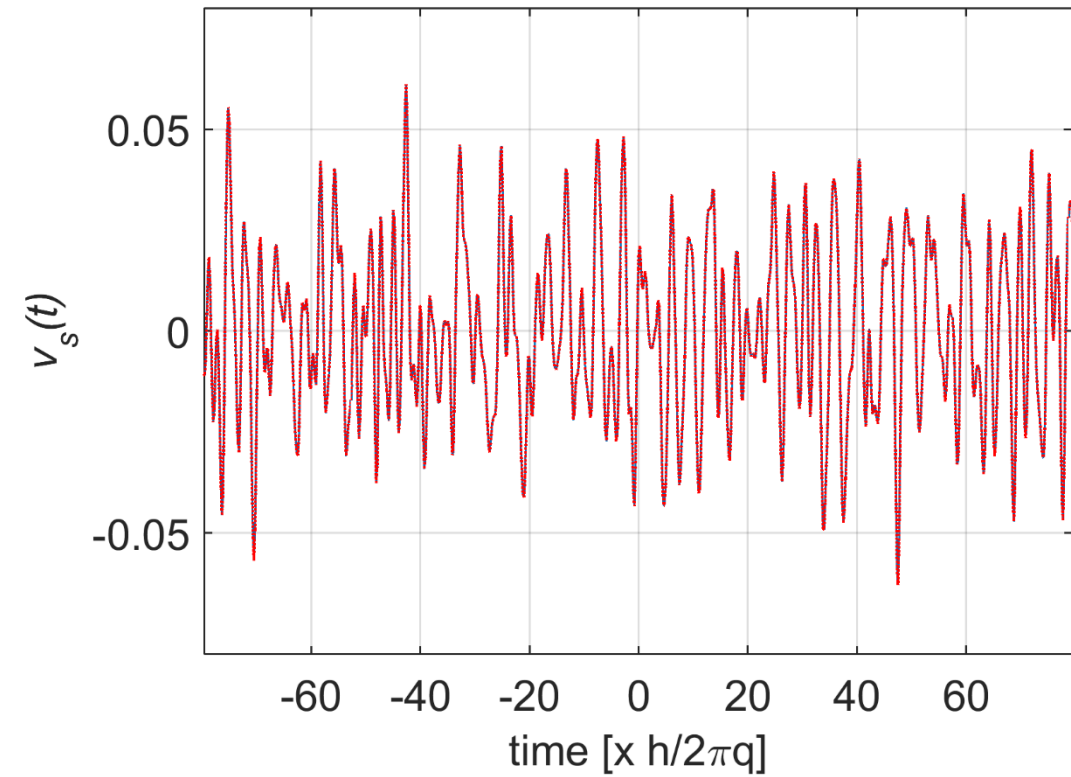
# Calculating broadband rectenna response for solar spectrum

Slide courtesy: Saumil Joshi, UC Boulder

### Frequency spectrum



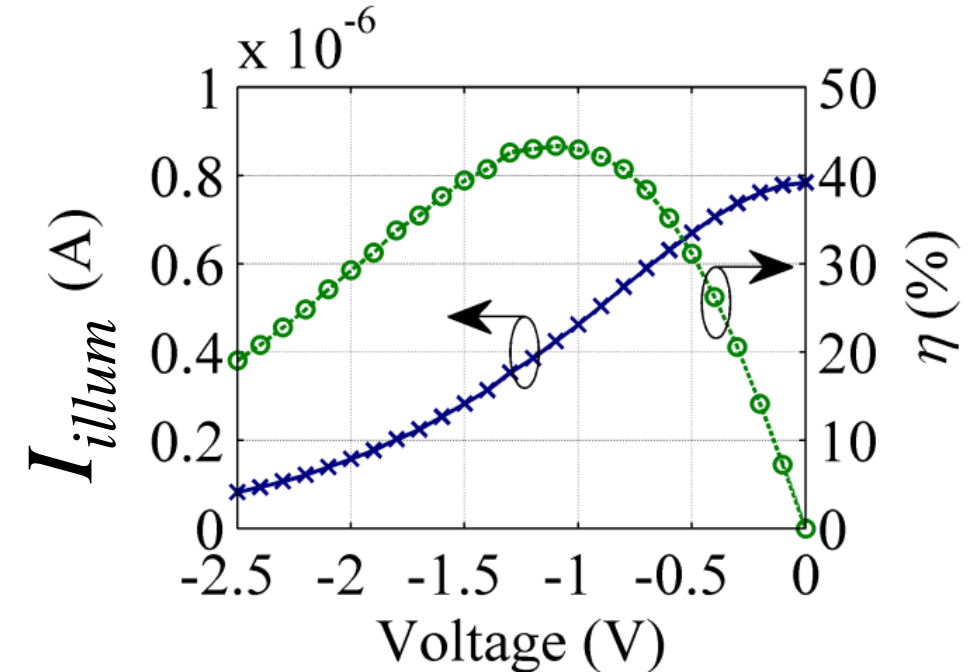
### Time-domain signal



# Efficiency limit for rectifying solar radiation (quantum regime)

Slide courtesy: Saumil Joshi, UC Boulder

- 5700 K blackbody
- 1000 W/m<sup>2</sup>
- Spatial coherence area ~19 μm
- Maximum power ~1.1 μW
- Quantum operation
- Peak efficiency ~ 44%
  - Matches Shockley-Queisser's ultimate efficiency limit

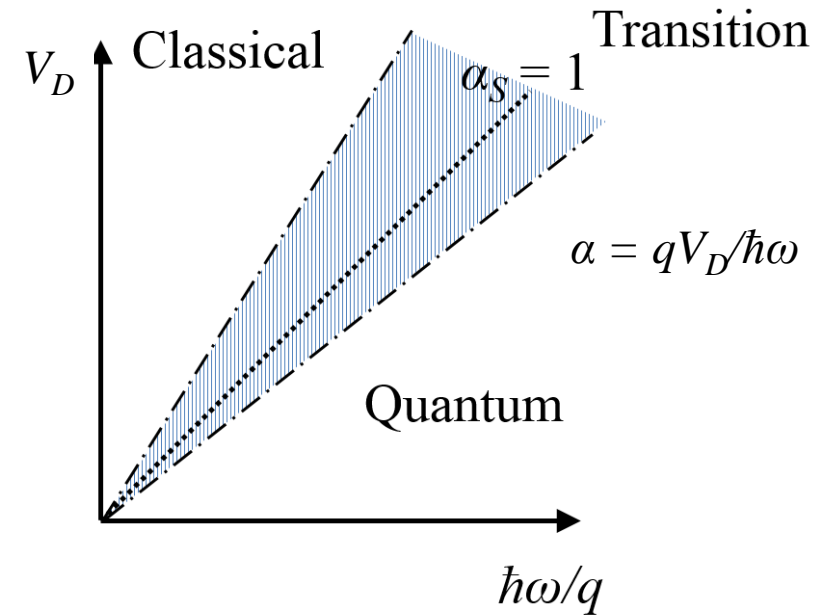


Joshi, Modell, Appl. Phys. Lett. 102, 083901 (2013)

# Can we exceed the 44% limit?

Slide courtesy: Saumil Joshi, UC Boulder

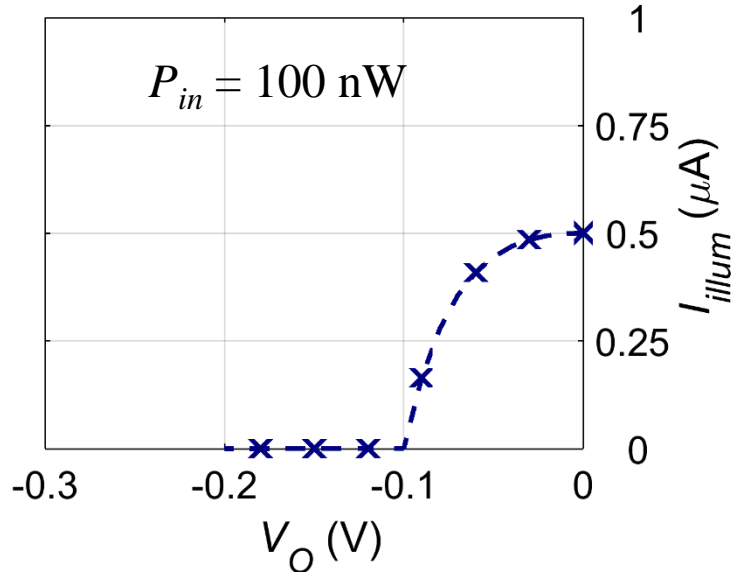
- Microwave rectennas > 70%
- Use low energy photons?
- Three regimes
  - Quantum ( $\alpha < 1$ )
  - Transition ( $\alpha \sim 1$ )
  - Classical ( $\alpha \gg 1$ )
- Increase diode voltage, relative to  $\hbar\omega/q$
- Two ways to reach classical operating regime
  - High input intensity
  - High radiation resistance





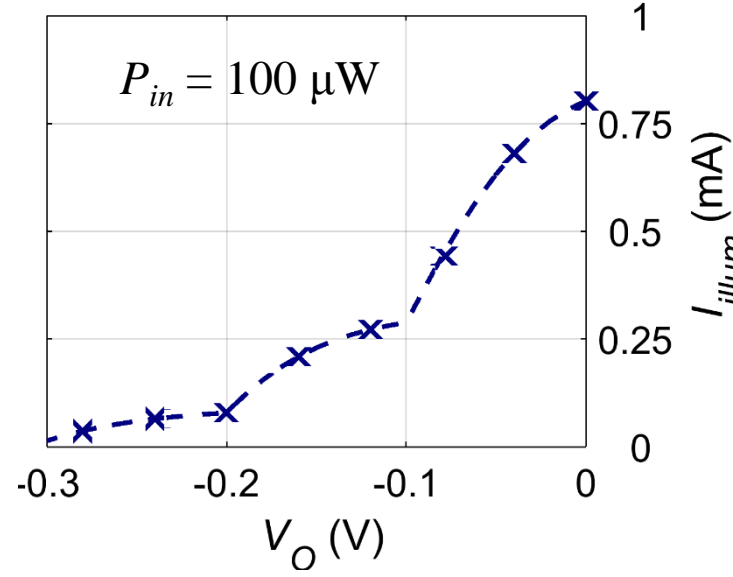
# Effect of input intensity on operating regime

Slide courtesy: Saumil Joshi, UC Boulder



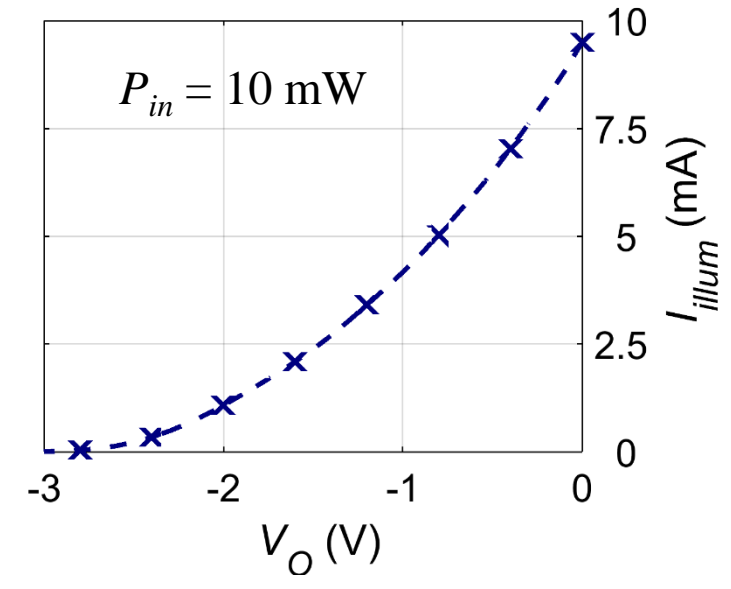
Quantum regime

- Low intensity, high frequency
- Frequency-dependent
- Hump observed



Transition regime

- Higher intensity, multiple photons
- Frequency-dependent
- Multiple steps



Classical regime

- Very high intensity
- Frequency independent
- Large number of photons

Joshi, Ph.D. Thesis, CU Boulder, 2015

# Conclusion: efficiency limits of optical rectennas



Slide courtesy: Saumil Joshi, UC Boulder

- Quantum operation
  - Low intensity, high frequency - single photon process
  - Monochromatic efficiency  $\rightarrow$  100%
  - Broadband efficiency maximum = 44%
  - Split-spectrum  $>$  44%
- (Quantum) classical operation
  - Possible at high frequencies through photon mixing  $\rightarrow$  large voltage operation
  - Broadband efficiency  $>$  44%
- Rectenna solar cell efficiency can exceed Shockley-Queisser limit
  - Through multi-photon process at high intensity
- Challenges
  - Coherence limits power
  - High diode resistance  $\rightarrow$  large  $RC$  time-constant
  - Diode breakdown

Thank you.

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